

1 **Fabrication and Characterization of Cellulose Acetate-Based Nanofibers and**
2 **Nanofilms for H₂S Gas Sensing Application**

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Abstract

31 Electrospun nanofibers and solution-casting nanofilms were produced from an environmentally
32 friendly cellulose acetate (CA) blended with glycerol (as an ionic liquid (IL)), mixed with
33 polypyrrole (PPy, a conducting polymer) and doped with tungsten oxide (WO_3) nanoparticles. The
34 sensing membranes fabricated were used to detect H_2S gas at room temperature and shown to
35 exhibit high performance. The results revealed that the lowest operating temperature of both
36 nanofiber and nanofilm sensors was 20°C , with a minimum gas detection limit of 1 ppm. Moreover,
37 the sensor exhibits a reasonably fast response, with a minimum average response time of 22.8 and
38 31.7 s for the proposed nanofiber and nanofilm based sensors, respectively. Furthermore, the
39 results obtained indicated an excellent reproducibility, long-term stability, and low humidity
40 dependence. Such distinctive properties coupled with an easy fabrication technique provide a
41 promising potential to achieve a precise monitoring of harmful H_2S gas in both indoor and outdoor
42 atmospheres.

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47 **Keywords:** Cellulose acetate, Polypyrrole; H_2S sensor; organic-inorganic hybrid nanocomposites.

48

49 **1. Introduction**

50 Environmental pollution has become a significant issue worldwide due to the growing industrial
51 waste emission to the community (Lu et al., 2017). Toxic gases such as hydrogen Sulfide (H_2S),
52 carbon monoxide (CO) and ammonia (NH_3) are recognized as environmentally dangerous gaseous
53 pollutants (Kaur et al., 2008; Marszałek, Kowalski & Makara, 2018; Ryu, Arifin, Ha & Lee, 2015).
54 H_2S is of a particular interest since it is one the most hazardous and harmful gases. H_2S is colorless,
55 highly toxic, poisonous, corrosive, flammable and explosive (Beauchamp et al., 1984). It is
56 progressively produced from the anaerobic decomposition of organic materials or other industrial
57 activities including food processing, cooking ovens, kraft paper mills, and petroleum refineries
58 (Ma et al., 2008; Sukunta et al., 2017; Gong et al., 2006). If inhaled, H_2S can cause
59 unconsciousness or death, even at very low concentrations (Mokhatab & Poe, 2012; Yamazoe,
60 2005).

61 Consequently, it is essential to monitor H_2S in different settings in real-time and develop highly
62 efficient H_2S sensors in-situ for both industrial and domestic applications (Sun, Yuan, Lium Han
63 & Zhang, 2005). Different methods have been developed to measure trace levels of H_2S in air. The
64 measurement techniques most widely used include gold film analyzers, SO_2 conversion,
65 colorimetric gas detection tubes, electrochemical detectors, and lead acetate cassette tape gas
66 detectors. However, each of them has clear advantages and drawbacks (Deuchar, 2003; Joshi et
67 al., 2014; Pandey, Kim & Tang, 2012; Miura, Yan, Lu & Yamazoe, 1996; Kroll, Smorchkov &
68 Nazarenko, 1994; Khan et al., 2017; Engel, Tarantik, Pannek & Wöllenstein, 2019).
69 Semiconducting metal oxides have been known for decades as good gas sensing materials because
70 of their high sensitivity to many target gases, low cost, and easy fabrication methods.
71 Semiconducting metal oxides (MOSs) such as (Fe_2O_3 , CuO, and WO_3) have been widely used for
72 gases and vapors sensing (Tiemann, 2007). In the last few years, nanostructures of metal oxides
73 were found to be effective as gas-sensing materials because of their high surface area that
74 contributes to improving significantly gas detection performance (Afzal, Cioffi, Sabbatini & Torsi,
75 2012; Sberveglieri et al., 2007; Mirzaei & Neri, 2016; Wetchakun et al., 2011). Among these,
76 WO_3 (tungsten oxide), an n-type metal oxide, exhibits compelling advantages for H_2S gas sensing
77 applications, by virtue of its structure, surface morphology, defect structure, and active surface
78 area, which greatly affect gas sensing properties (Wang et al., 2016; Yin et al., 2019; Kim et al.,
79 2018). However, MOS-based gas sensors including WO_3 suffer mainly from high operating

80 temperatures (~150–300 °C) that lead to high power consumption and result in a short lifetime
81 [Ali *et.al.*, 2019]. In recent years, different strategies for room-temperature operation using
82 especial morphologies have been introduced in an attempt to address the issue of high-power
83 consumption for resistance-based sensors [Sanjit *et.al.*, 2021]. One of these strategies involves the
84 development of new sensors based on organic conducting polymers with the functionality and
85 conductivity level required to improve gas sensing performance. Such efforts aim at reducing
86 electrical power consumption using low temperatures to maintain their long-term performance and
87 to achieve large-scale production [Kaushik, *et.al.*, 2015]. Intrinsically conducting polymers
88 (ICPs), the so-called “fourth generation of polymeric materials” have been recognized as a new
89 class of organic conducting polymers with remarkable mechanical and electrical properties
90 (Heeger, 2001). ICPs, such as polyacetylene (PA), PPy and polyaniline (PANi) contain monomers
91 that are capable of gaining positive or negative charge through oxidation or reduction. This
92 phenomenon largely contributes to the intrinsic electrical conductivity of the ICPs (Abdelhamid
93 & Snook, 2002; Nambiar & Yeow, 2011). ICPs play an important role in different commercial
94 applications, particularly in actuators, sensors, and electrochromic devices (Smela, 1999; Van de
95 Leur & Van der Waal, 1999; Kincal, Kumar, Child & Reynolds, 1998). For instance, significant
96 research effort has been devoted to PPy due to its good environmental stability, easy synthesis and
97 greater conductivity compared to other ICPs (Ma, Sg, Pr & Shashwati, 2011; Cho et al., 2005).

98 On the other hand, ionic liquids (ILs) are considered as promising materials for numerous
99 applications (Shokouhi, Adibi, Jalili, Hosseini-Jenab & Mehdizadeh, 2010). Generally, ILs are
100 well known for their good ionic conductivity attained at room temperature and low vapor pressure
101 values (Wei & Ivaska, 2008; Nádherná, Opekar, Reiter & Štulík, 2012; Li, Liu, Pei, Wang & He,
102 2012). Furthermore, ILs are considered environmentally friendly materials (Li, Liu, Pei, Wang &
103 He, 2012). Such exclusive properties make ILs suitable for the production of electrochemical
104 sensors (Ayesh, Abu-Hani, Mahmoud & Haik, 2016) but also to enhance the ionic conductivity of
105 less conductive polymer (Ayesh, Qadri, Baboo, Hai & Haik, 2013).

106 Significant research has been directed toward employing nanostructured materials for gas
107 sensing applications. Among various classes of nanostructures, one-dimensional nanomaterials,
108 e.g. “nanofibers (NFs)”, exhibit an excellent potential for use in gas sensing due to their large
109 surface-to-volume ratio and high interconnected porosity [Ramakrishna *et.al.*, 2006, Mercante *et.*
110 *al.*, 2019]. This work focuses on producing nanofibers from semiconducting organic polymer

111 blended with inorganic metal-oxide nanoparticles to detect H₂S gas at low temperature and low
112 detection limit. The sensors fabricated operate at room temperature with detection a limit of 1 ppm
113 and a fast response time of 22.8 - 31.7 s.

114 In our previous studies, hybrid (inorganic-organic) membranes were successfully developed and
115 evaluated as H₂S gas sensors. In these studies, combinations of semiconducting nanoparticles
116 (WO₃ and CuO) were used in a matrix of a conductive polymer (Chitosan, PVA) and with the help
117 of an ionic liquid, synergistically provided a mechanism of detecting H₂S gas at low temperatures.
118 The proposed sensor assembly is an organic-inorganic nanocomposite, i.e. a hybrid structure that
119 has attracted much attention for the development of sensing applications (Wang & Shannon, 2011).
120 The uniqueness and novelty of the proposed hybrid structure is in the combined contribution of its
121 carefully selected components and the conducting nature of the environmentally friendly and
122 sustainable CA and to the role played by the ionic liquid acting as a facilitator of charge transfer
123 within the matrix (Ju, Park, Jung & Lee, 2009; Allam, Ayesh, Mohsin & Haik, 2013). Moreover,
124 the presence of intrinsically conducting PPy particulates and semiconducting WO₃ nanoparticles
125 ensures a smooth charge transfer and provide an added value for the overall sensor construct (Geng
126 et al., 2006; Su & Peng, 2014; Ali, Awwad, Greish, Abu-Hani & Mahmoud, 2020; Abu-Hani,
127 Greish, Mahmoud, Awwad & Ayesh, 2017). Furthermore, the sensor fabricated in our previous
128 work [Hittini et. al., 2020] is highly affected by the relative humidity and the response of the sensor
129 was around 12% at 20% relative humidity. The current sensors exhibited a low humidity
130 dependence, and the responses of the nanofiber and nanofilm-based sensors are 15% -20% at 80%
131 humidity, respectively. Thus, this sensor has the potential to work in a harsh environment. The
132 proposed sensor assembly is shown to exhibit enhanced features compared with similar sensors
133 reported in the literature.

134 **2. Experiment**

135 **2.1. Materials**

136 Tungsten Oxide (WO₃, 99% hydrolyzed), cellulose acetate (CA, MW 50,000 and 35% acetyl
137 content), polypyrrole (PPy, conductivity 10-50 S/cm), acetone, dimethylacetamide (DMAc), and
138 glycerol (IL) were purchased from Sigma Aldrich-USA.

139 **2.2. Preparation of (PPy-IL- WO₃ NPs-CS) solution**

140 Composite sensor mixtures were prepared in three separate 100-ml beakers based on the WO₃ NPs
141 proportions. In each beaker, 0.24 g of glycerol (IL) was added to 40 ml of DMAc/Acetone (1:2)

142 solvent mixture and thoroughly mixed. 5, 7.5, and 10 wt.% of WO_3 NPs (in proportion to CA
143 used) were subsequently added to the individual solutions to vary the concentration of WO_3 NPs.
144 This was followed by the addition of PPy, 2wt.% with respect to CA used before magnetic stirring
145 was applied until homogeneous suspensions were obtained. 4.8 g of CA was gradually and slowly
146 added (time of addition is 5 hours) to each suspension and subjected to a continuous vigorous
147 stirring for 24 h until clear homogeneous solutions were achieved. The amount of IL used was
148 calculated to be 5wt.% of CA while the CA concentration was 12wt.% of the solution's total
149 volume. The solutions prepared were used for the fabrication of nanofilm and nanofibers-based
150 sensor membranes denoted hereafter as PPy-IL- WO_3 NPs-CA.

151 **2.3. Preparation of (2 wt% PPy-IL-10 wt% WO_3 -CA) nanofilm-based sensor**

152 To prepare the sensing nanofilms with different WO_3 concentration, a fixed volume of each of the
153 homogenous solutions was cast on a Teflon plate to form a thin membrane, then dried in a vacuum
154 oven at 50°C for 12 h. A non-porous cast film with a high degree of flexibility was obtained, as
155 shown in Fig. 1. Uniform composite membranes of around 1.7 mm thickness were obtained.

156 **2.4. Preparation of (2 wt% PPy-IL-10 wt% WO_3 -CA) nanofiber-based sensor**

157 To prepare the fibers, a constant volume of 10 ml of each of the homogenous solutions was fed
158 into a plastic syringe, then electrospun into nanofibers at ambient conditions using
159 NANOSPINNER24 equipment. A set of pre-optimized electrospinning parameters was used,
160 including a stainless steel needle with 21 gauge, a spinning distance (needle tip to collector
161 distance) of 15 cm, an applied voltage of 20 kV between the tip and the grounded collector, and a
162 constant flow rate of 0.5 ml/h. The electrospun fibrous membranes obtained were in the form of
163 flexible sheets, which were dried further at 50°C for 12 h.

164 **2.5. Characterization**

165 The morphologies of the as-received PPy powder and the nanofibrous films prepared thereafter
166 were investigated using scanning electron microscopy (SEM: JEOL, JSM-5600). In addition, an
167 energy-dispersive X-ray spectrometer (EDS) was used to confirm the presence and the
168 homogeneity of the WO_3 -PPy-CA composite fibrous membranes. The size of the WO_3 particle
169 was obtained using a Zetasizer (Malver Instruments, Model ZEN360, United Kingdom).

170 **2.6. Sensor fabrication**

171 Each sensor was fabricated and connected electrically as explained elsewhere (Abu-Hani, Awwad,
172 Greish, Ayesh & Mahmoud, 2017). A square piece (1×1 cm²) of the composite film/fiber was cut

173 and placed between a 0.15 μm thick copper bottom contact ($1.5 \times 1.5 \text{ cm}^2$) and a stainless steel grid
174 ($0.8 \times 0.8 \text{ cm}^2$) with a mesh size of $250 \times 250 \mu\text{m}^2$ as the top contact. Stainless steel was chosen for
175 the top contact because it is anti-corrosive, therefore, resistant H_2S . A conductive silver paste was
176 used to fix the three layers, acting as an efficient heatproof adhesive.

177 **2.7. H_2S Gas sensing test**

178 The sensor fabricated was placed on a hot plate inside a temperature-controlled Teflon chamber.
179 The bottom and top parts of the device were connected by 2 electrical feed-troughs. Furthermore,
180 a Bronkhorst mass flowmeter was used to control the flow rate of the gases. Before the injection
181 of the H_2S gas into the chamber, the gas was diluted with a fixed proportion of air with flow rate
182 of 200 sccm using a gas mixer such that the concentration of the H_2S gas becomes 1, 10, 15, 25
183 and 50 ppm. The sensors developed were subsequently exposed to H_2S inside the temperature-
184 controlled Teflon chamber. The tests were conducted under atmospheric pressure inside a fume
185 hood and at different temperatures 20, 40, and 60°C (measured at the copper sheet's surface). All
186 tests (current-voltage: I-V) were performed by applying a fixed bias voltage of 2.0 V across the
187 sensor electrodes and the electrical current was measured as a function of time using a Keithley
188 Instruments source measurement unit (KI 236). All I-V measurements were performed in
189 triplicates ($n=3$) to ensure a statistical relevance of the data recorded. The gas flow meters,
190 controller, and KI 236 were interfaced to a computer using LABVIEW software. The relative
191 humidity inside the test chamber was 0% (dry gas) unless stated otherwise. A detailed schematic
192 diagram of the gas testing system is provided in our previous work (Hittini et al., 2020).

193 **3. Results and Discussion**

194 **3.1. Morphology and structural characteristics**

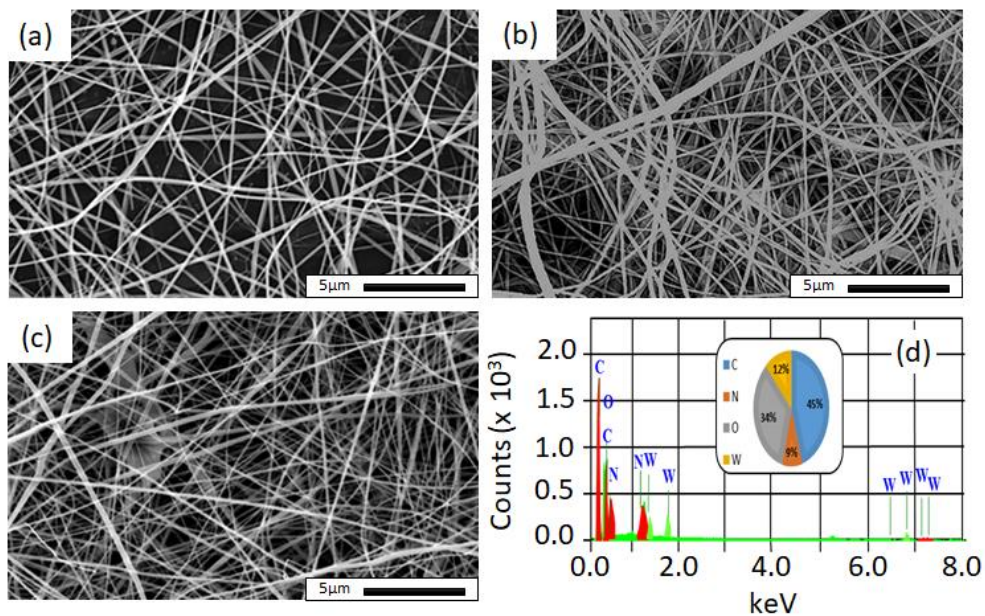
195 The as-received PPy conducting polymer was analyzed for its structure and composition using
196 SEM-EDS. The PPy particulates showed a uniform granularity with a high purity and an elemental
197 composition of C and N, as confirmed by the EDS analysis. The average size of the PPy
198 particulates is approximately $0.9 \mu\text{m}$, with a unimodal particle size distribution obtained by particle
199 size analysis. The WO_3 NPs used in this work were characterized for their composition and
200 morphology in our previous study (Ali, Awwad, Greish, Abu-Hani & Mahmoud, 2020). The
201 average size of the WO_3 NPs was 140-200 nm, as measured by Diameter J software (Ali, Awwad,
202 Greish, Abu-Hani & Mahmoud, 2020).

203 To produce a non-beaded nanofibrous sensor membrane, the optimum proportion of PPy initially
204 added to the CA solution prior electrospinning was evaluated. Accordingly, three PPy
205 concentrations; 2, 5, and 7wt.%, were studied. An optimum proportion of 2wt% of the PPy
206 particulates was selected since non-beaded nanofibers with a homogeneous fiber size distribution
207 were achieved thereafter. However, increasing the proportion of the PPy particulates resulted in
208 the presence of beads in the nanofibrous films. This is attributed to the increased viscosity of the
209 PPy-CA suspension with the addition of PPy particulates, which in turn affects the
210 electrospinnability of the suspension (Jeun et al., 2007). This optimum PPy particulates
211 concentration was used for the preparation of the nanofibrous and nanofilm membranes at constant
212 IL and CA concentrations for 5, 7.5, and 10wt.% WO_3 NPs intake.

213 Fig. 1(a-c) show the SEM micrographs of the CA nanofibrous electrospun membranes containing
214 2wt.% PPy and 5 vol.% IL for three different concentrations of WO_3 NPs (5, 7.5, and 10wt.%
215 WO_3). Increasing WO_3 concentration from 5 to 10wt.%, causes an increase in the initial viscosity
216 of the solutions, which was reflected in an increase in the fiber's diameter, as illustrated by Fig. 1.
217 It is a well-known fact that the diameter of the nanofibers fabricated by electrospinning are greatly
218 influenced by the polymer concentration and the viscosity of the solution. Under the same
219 electrospinning conditions, increasing the polymer concentration causes an increase in solution
220 viscosity. Hence, increasing the viscosity of the solution increases the diameter of the nanofibers
221 [J. Lasprilla-Botero, M. Álvarez-Láinez, and J.m.Lagaron, 2018, Y. Yang, R. He, Y. Cheng, and
222 N. Wang, 2020]. Composite membranes containing 5 and 7.5wt% WO_3 are characterized by an
223 average fiber size of 350 nm and 500 nm, respectively. However, a membrane with 7.5wt% WO_3
224 exhibited a heterogeneous fiber size distribution. In turn, 10wt% WO_3 in the nanofibrous
225 membrane led to 400 nm average fiber size with a homogeneous fiber size distribution. On the
226 other hand, the increase in the dimensions of the nanofibers led to a decrease in the porosity of
227 the membranes. These results are in a good agreement with the data presented in our previous work
228 [Hittini et., al., 2020]. Moreover, increasing the concentration of WO_3 NPs to 10wt% led to an
229 increase in the reactive sites within the fibrous sensing membrane and hence improves the response
230 of the sensor. Therefore, the sensors made with 10wt% WO_3 shows a noticeable improvement in
231 the sensor's response due to high porosity and more reactive sites in the sensing membrane
232 compared with 5 and 7.5wt% of WO_3 NPs. The presence of the WO_3 NPs and PPy particles was
233 further confirmed by elemental analysis (EDS) of the fibrous membrane containing the highest
234 concentration of WO_3 NPs (10wt.%), as shown in Fig. 1(d). Accordingly, an optimum

235 concentration of 10wt.% of WO_3 NPs in the CA fibrous membranes was selected to study the
236 sensing characteristics of the membranes prepared.

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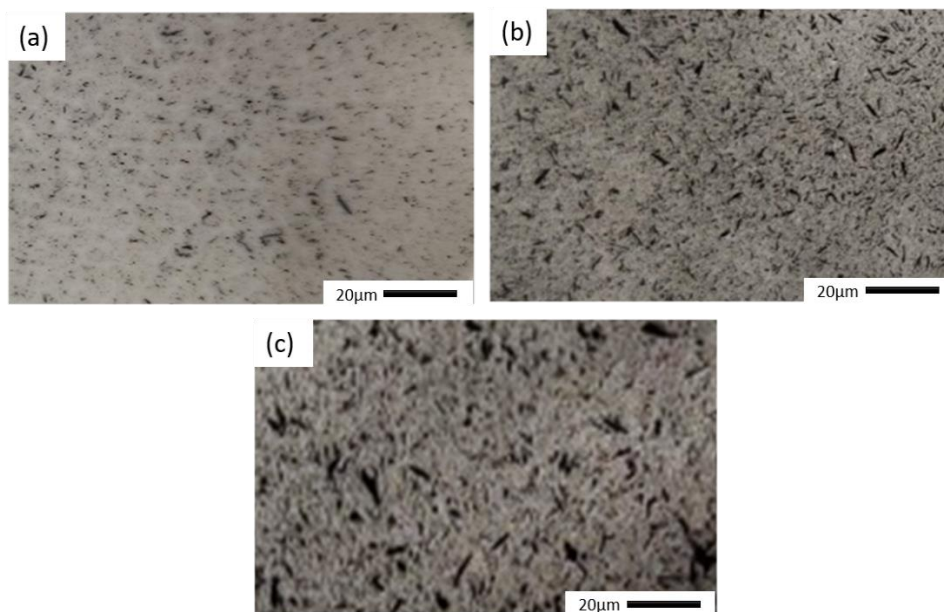


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Fig. 1. SEM images of (a) PPy-IL-5wt% WO_3 -CA nanofibers. (b) PPy-IL-7.5wt% WO_3 -CA nanofibers, (c) PPy-IL-10wt% WO_3 -CA nanofibers, and (e) EDS spectra of PPy-IL-10wt% WO_3 -CA nanofibers.

239

240 Fig. 2(a-c) show the microstructure of the nanofilms prepared, with an approximate average
241 thickness of 1.7 mm. In addition, all nanofilms showed the same degree of flexibility, while a
242 homogeneous distribution of the PPy and WO_3 particles was confirmed.

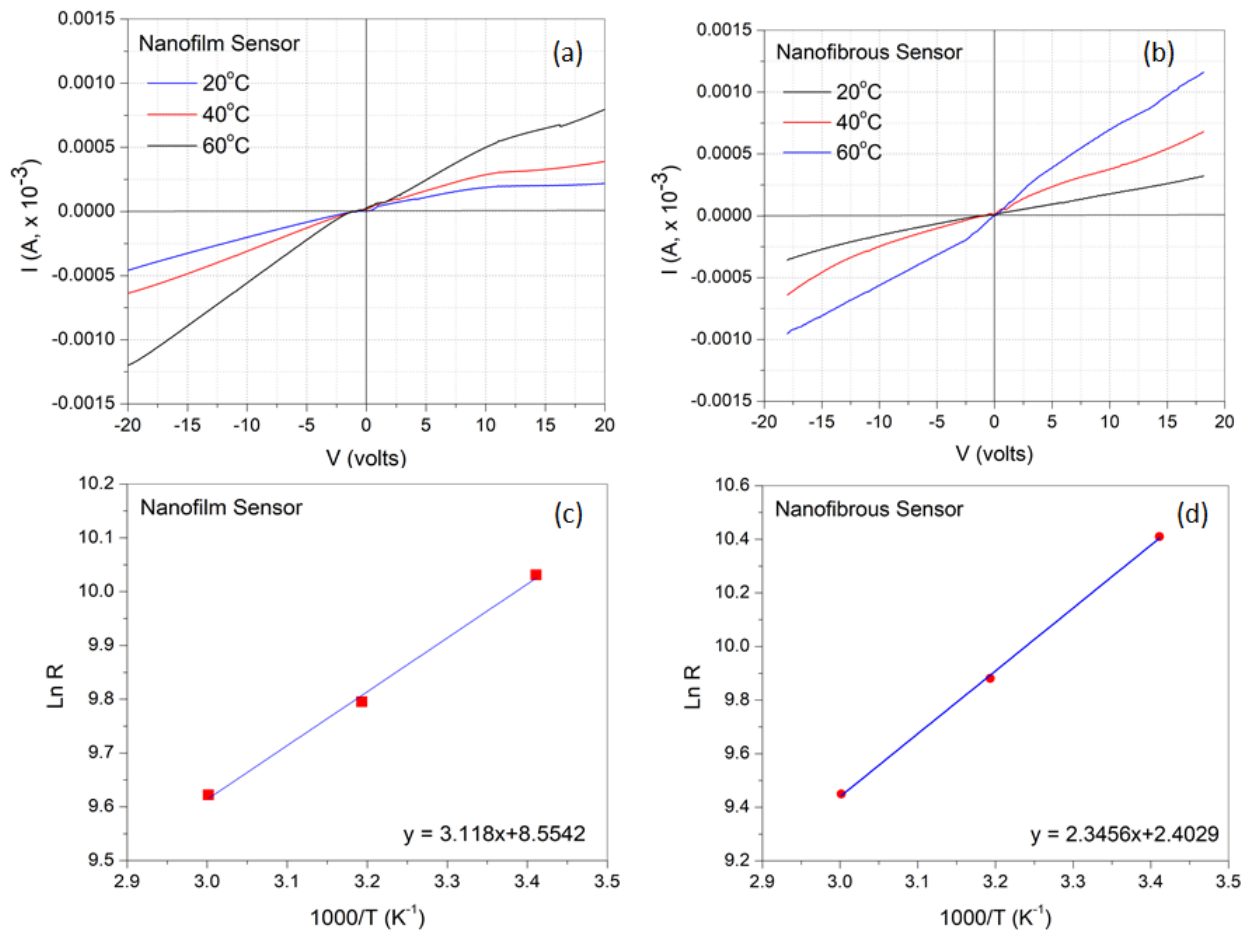


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244 Fig. 2. SEM micrographs of the prepared sensing nanofilms containing; (a)10wt% WO_3 , (b)
245 7.5wt% WO_3 , and (c) 5wt% WO_3 .

246 3.2. Electrical characteristics

247 Since the operating temperature plays a major role in the gas sensing performance, the I-V
248 characteristics of the composites prepared were evaluated at three different operating temperatures:
249 20, 40, and 60°C. Fig. 3 (a & b) displays typical I-V curves as a function of temperature for the
250 PPy-IL-10wt.% WO_3 -CA nanofilm and nanofiber samples, respectively. These I-V curves are
251 almost linear but have a slight nonlinearity and vary with the operating temperature as expected.
252 Such I-V performance is attributed to the increase in the electrical charge carriers conduction path
253 induced by the addition of IL and the NPs. This is in line with the small potential barrier observed
254 between the contact and the polymer membrane (Liu, Adhikari, Guo & Adhikari, 2013). In
255 addition, the PPy conductive polymer particulates present in the polymer matrix also contributes
256 to increasing the conductivity observed. Such phenomena facilitate charge carriers transport once
257 the sensor is exposed to H_2S gas (Nguyen & El-Safy, 2011; Ayesh, Mahmoud, Qamhieh & Karam,
258 2014).



259 Fig. 3. Electrical characteristics of (2 wt% PPy-IL-10 wt% WO_3 -CA) sensors; (a) I-V curve for
 260 nanofilm sensor. (b) I-V curve for nanofiber sensor. Dependence of the resistance ($\ln(R)$) on the
 261 temperature ($1000/T$) for nanofilm based sensor (c) and nanofiber-based sensor (d).
 262

263 linearly as the temperature increases, which is attributed to the increase in the number of the free
 264 charge carriers in the conduction band due to thermal excitation (Mironenko et al., 2016).
 265 Consequently, a linear fit of the curves was used to determine the activation energy (E_a) of each
 266 sensor following Arrhenius equation (Eq. 1) (Jensen, 1985):

$$267 \quad R = R_0 e^{\frac{E_a}{k_B T}} \quad (1)$$

268 Where, R_0 is a pre-exponential factor, k_B the Boltzmann constant, and T the temperature. The
 269 activation energy extracted for the nanofilm and nanofiber-based sensors were 0.270 and 0.202
 270 eV, respectively. The relatively lower activation energy for the nanofiber sensor compared with

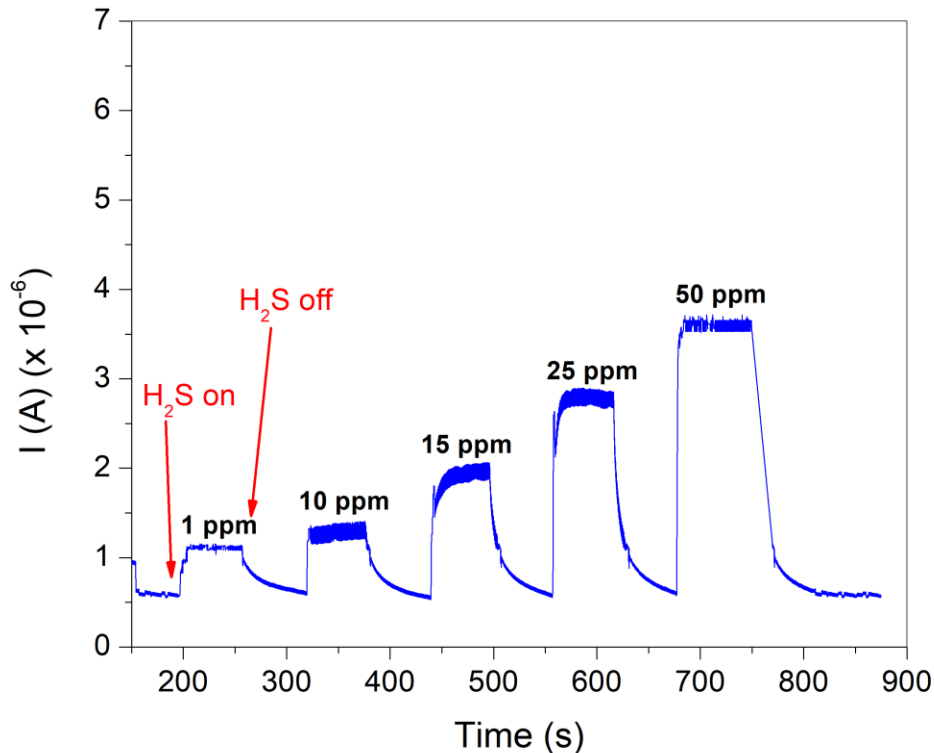
271 that of the nanofilm sensor could be attributed to the higher surface area of the nanofibers sensing
272 element as compared with that of the nanofilm sensing element, even though both sensing elements
273 contain the same constituents. As a first approximation, the activation energy can be seen as the
274 difference between the conduction band and the Fermi energy level, $E_a = E_C - E_F$. Since the surface
275 area of the nanofiber-based sensor is bigger than that of the nanofilm-based sensor, a higher surface
276 defect states are expected. The creation of these defects alters the density of states in the forbidden
277 energy gap, which shifts the Fermi level towards the conduction band edge and lowers the
278 activation energy as a result. It should be mentioned that low activation energies are highly
279 desirable since it enhances the sensor's response to H₂S gas presence and recovery time while
280 decreasing the operating temperature (Korotcenkov, 2007). The low activation energies observed
281 could be attributed to the inter-particle electron movement from WO₃ to PPy at the heterojunctions,
282 where a positively charged depletion layer is formed on the WO₃ surface. This phenomenon, not
283 only contributes to the reduction of the activation energy, but it also results in a reduction in the
284 enthalpy of the physical adsorption of gases, thus showing excellent electron-donating
285 characteristics (Geng et al., 2006; de Lacy Costello, Evans, Ewen, Honeybourne & Ratcliffe,
286 1996).

287 Depending on the data shown in Fig. 3 (a & b), a constant biased voltage (2.0 V) was calculated
288 from the linear part of the I-V curves, and was applied across the sensors' electrodes in order to
289 avoid any current saturation (Ali, Mahmoud, Awwad, Greish & Abu-Hani, 2020). Accordingly,
290 the I-V response was measured as a function of the gas concentration, time and temperature as
291 shown later in the current study.

292 **3.3. Gas sensing properties**

293 The performance of the nanofiber and nanofilm sensors obtained with the chemical composition
294 of PPy-IL-10wt.% WO₃-CA was investigated for the detection of H₂S gas. The sensor was
295 prepared and inserted inside the gas test chamber as discussed in section 2.7. A fixed bias of 2.0
296 V was applied to establish a background current in the sensor before the sensor was exposed to for
297 different concentrations of H₂S gas (1-50 ppm). The corresponding current response signal was
298 measured as a function of time. Fig. 4 represents the sensor's time dependent-current response at
299 40°C for the PPy-IL-10wt.% WO₃-CA nanofiber sample. These results indicate that the current
300 measured increases significantly, as the sensor is exposed to increasing concentrations of H₂S.
301 These changes in the current correspond to a decrease in the resistance, which is attributed to the

302 proton doping effect associated with PPy particulates and is further supported by the characteristics
 303 of WO₃ NPs as an established n-type semiconductor (Geng, 2010).



304
 305 Fig. 4. A representative current response of the (PPy-IL-10 wt% WO₃-CA) nanofiber-based
 306 sensor as function of the time and H₂S concentrations.

307 Furthermore, a reversible behavior of the sensor performance is clearly revealed, where the current
 308 recovers its initial value once the H₂S gas flow is closed and the residual H₂S pumped out. This
 309 behavior demonstrates the reproducibility of the sensors fabricated and the ability to use them
 310 several times without adversely altering their accuracy. Fig. 4 also indicates very clearly that the
 311 magnitude to the sensor's response is proportional to the gas concentration, where the higher the
 312 H₂S gas concentration, the higher the current value measured. The sensor's response to H₂S is
 313 defined by Eq. 2 and calculated at each operating temperature:

$$314 \quad S(\%) = \frac{|I_g - I_a|}{I_a} \times 100 \quad (2)$$

315 Where, I_a is the reference current of the sensor measured in air, and I_g the current of the sensor
 316 exposed to the test gas (mainly H₂S).

317 During the test, H₂S was diluted with air inside the gas mixer and injected into the test chamber at
 318 various H₂S concentrations: 1-50 ppm. Furthermore, the flow rate was controlled, while the

319 operating temperature was varied at 20, 40, and 60°C. Fig. 5 (a & b) displays the sensor's response
320 (S%) as a function of operating temperature and H₂S concentrations for both nanofibers and
321 nanofilms-based sensors, respectively. All measurements were performed in triplicates at a fixed
322 temperature and gas concentration.

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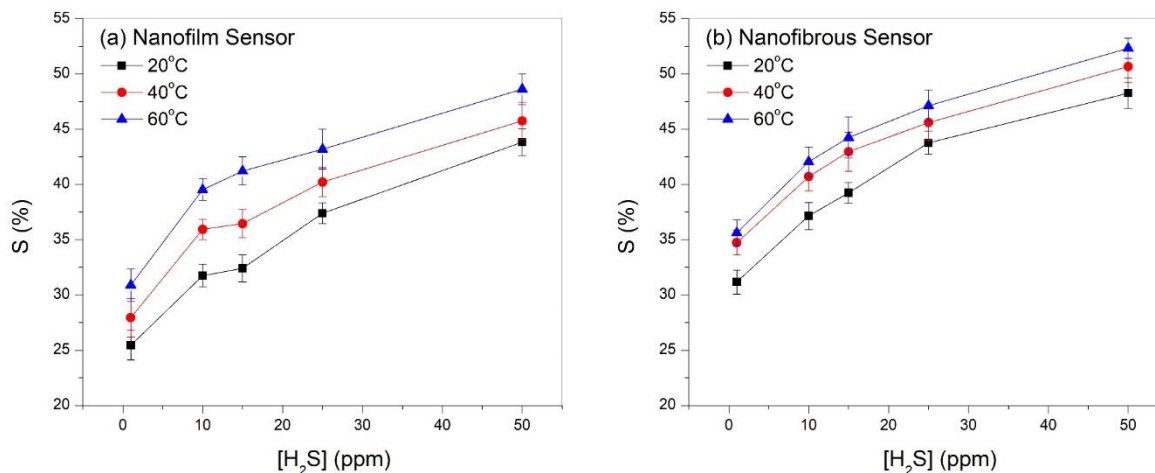
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330 Fig. 5. Sensor's response for H₂S gas of: (a) (PPy-IL-10 wt% WO₃-CA) nanofilm base sensor,
331 and (b) (PPy-IL-10 wt% WO₃-CA) nanofiber based sensor, at different H₂S concentrations and
332 operating temperatures.

333 The results show a high response to H₂S gas, even at a low temperature of 20°C. Likewise, the
334 response of the sensors is directly proportional to the gas concentrations and temperatures inside
335 the test chamber. For instance, as Fig. 5 (b) demonstrates that when the H₂S concentration was
336 increased from 10 to 25 ppm at a constant operating temperature, the response increases by 17.7%.
337 Whereas, at a constant H₂S concentration the sensor's response showed an increase of 13.2% when
338 the temperature was increased from 20 to 40°C. This could be attributed to the presence of both
339 WO₃ NPs and PPy particulates, which largely contribute to the conductivity of the sensor that is
340 further improved by increasing the operating temperature (Abu-Hani, Greish, Mahmoud, Awwad
341 & Ayesh, 2017). These results also indicate a high reliability of the sensor fabricated as the error
342 bars of the sensor's response are within a low standard deviation. A minimum detection limit of 1
343 ppm was achieved at all operating temperatures. It is very essential to notice a reasonable response
344 at low temperature (20°C) for all sensors fabricated, making the proposed sensor membranes
345 suitable to detect very low H₂S concentrations. As such these sensors can protect workers running
346 the risk of a direct and dangerous exposure to H₂S on daily basis.

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348

349 3.4. Sensor performance

350 To confirm the reliability of the sensors produced, four parameters were evaluated, i.e. selectivity,
351 response time, stability (reproducibility) and humidity. Each sensor was tested individually in
352 triplicates (n=3). The response time is a very significant criterion to evaluate the performance of
353 the sensors obtained. The response time is defined as the time needed to reach 90% of the sensor's
354 maximum response. Fig. 6 (a & b) presents the response time for the nanofilm and nanofiber-based
355 sensors as a function of the temperature and WO₃ NPs intake in both types of sensors. These results
356 indicate that the nanofilm-based sensor show a minimum average response time of 24.49 s at 60°C,
357 and a maximum average response time of 31.65 s at 20°C. On the other hand, the nanofiber sensor
358 showed a shorter minimum average response time of 16.56 s at 60°C, and a maximum average
359 response time of 22.81 s at 20°C. The faster response time for the nanofiber-based sensor is
360 attributed to the higher surface area of the sensing material, unlike the non-fibrous nanofilm sensor.
361 However, it should be noted that the response of the sensors developed are faster than those
362 mentioned in the literature for similar sensors used for the detection of H₂S gas (Geng et al., 2006;
363 Su & Peng, 2014).

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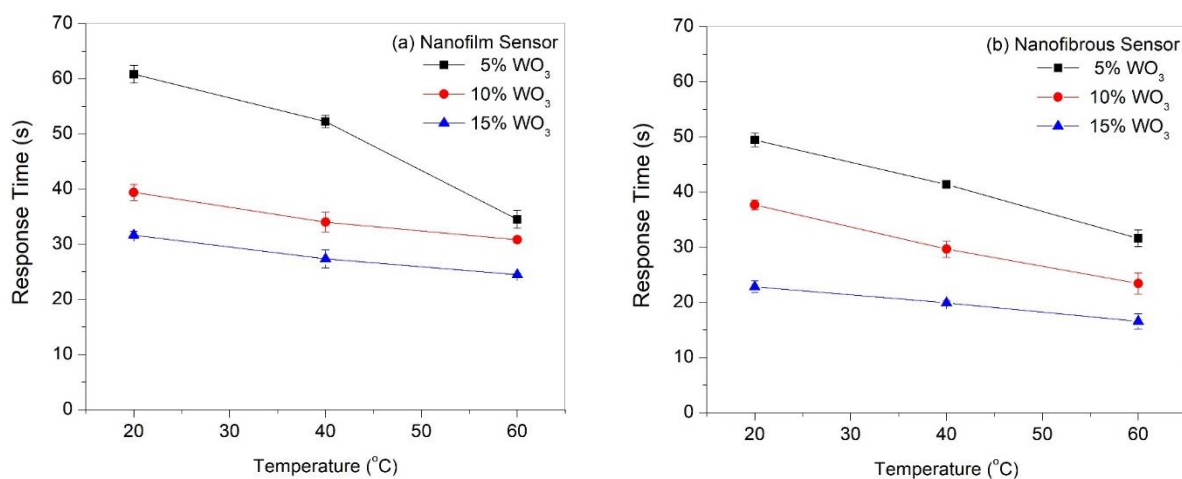
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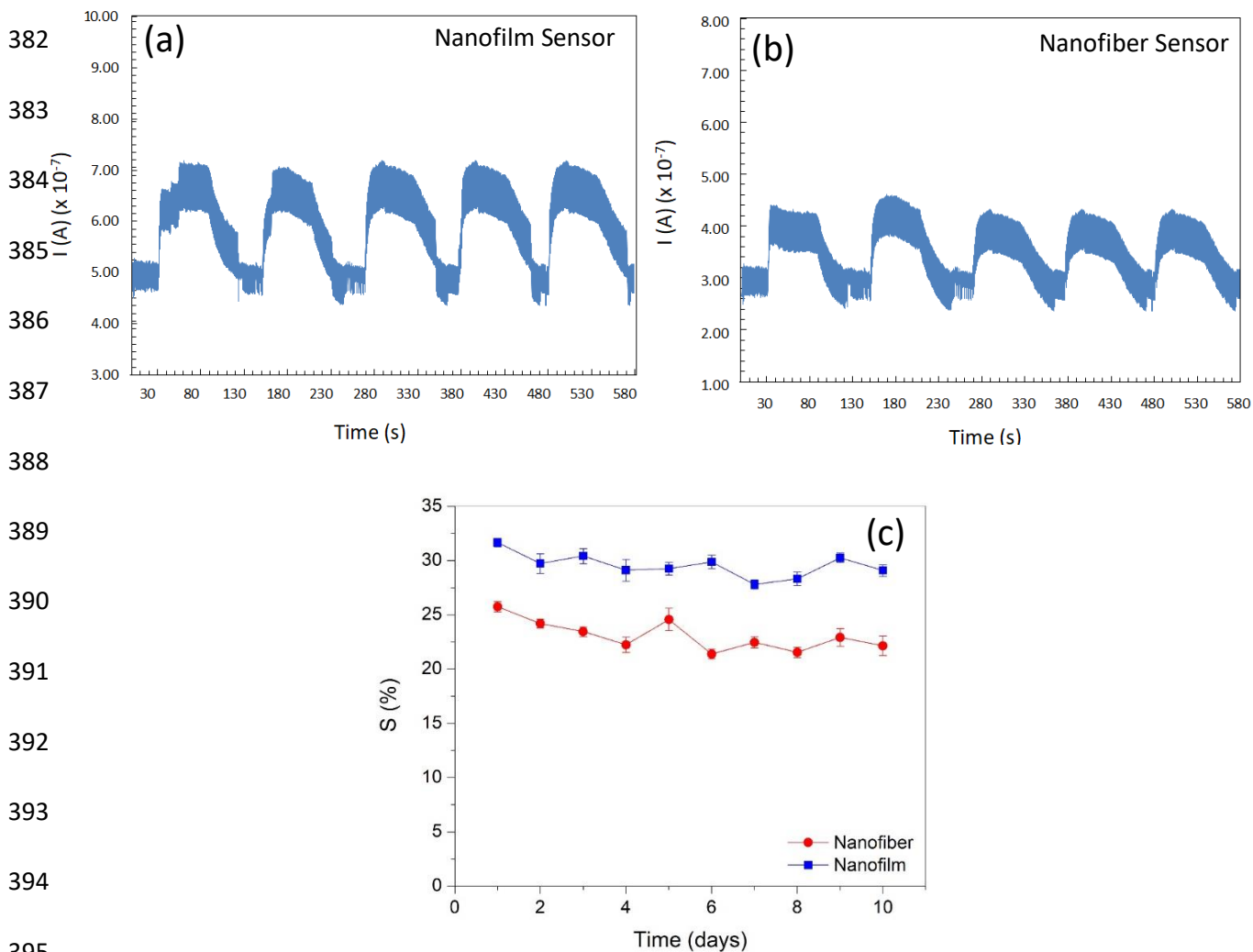


371 Fig. 6. Response times of the sensors as a function of temperature and WO₃ content for (a) CA-
372 PPy-IL-WO₃ nanofilm based sensor and (b) CA-PPy-IL-WO₃ fiber-based sensor.

373

374 To test the reproducibility of the fabricated sensors, each sensor was exposed to a constant H₂S
375 gas concentration of 10 ppm at a constant operating temperature of 40°C for four repeating cycles.
376 The results shown in Fig. 7 (a & b), suggest the responses of the sensors are broadly repeatable

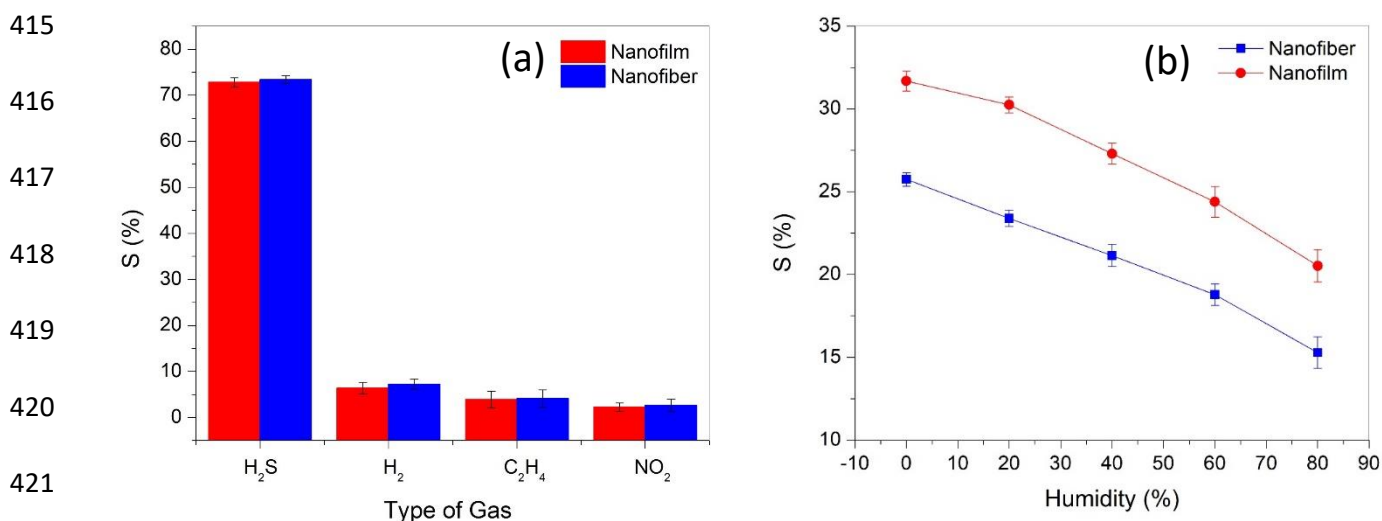
377 over the four cycles considered for both types of sensors. This is indicative of their good
 378 reproducibility in the detection of H₂S. This test was repeated continuously for 10 days and the
 379 response (S%) was calculated and presented in Fig. 7(c). For a given temperature and H₂S gas
 380 concentration, the repeated response of each sensor was very close to the initial response recorded,
 381 which indicates that both sensors fabricated exhibit an excellent long-term stability.



396 Fig.7. (a) Reproducibility of (PPy-IL-10 wt% WO₃-CA) nanofilm sensor (a) and (PPy-IL-10
 397 wt% WO₃-CA) fiber sensor. (c) Long-term stability of both sensors measured at 40°C.

398
 399 The selectivity of both sensors was tested, and the results shown in Fig. 8a. The sensors were
 400 exposed to three potential interfering gases separately, i.e. hydrogen (H₂), ethylene (C₂H₄), and
 401 nitrogen dioxide (NO₂) with a concentration of 200 ppm. The sensor's response to each of these
 402 gases was recorded at 40°C. The response (S%) of both sensors to all these gases are very weak
 403 (less than 10%), while their response to H₂S was exceptionally high (7-10 times higher), indicating

404 the high selectivity of the sensors proposed to H₂S gas. The relative humidity limits the reliability
 405 of the sensor to detect H₂S gas, since the ambient humidity varies dynamically with changes in the
 406 weather, season, and temperature. As such, reducing the dependence of the sensor on the humidity
 407 to a low level is highly desirable. The effect of varying the relative humidity inside the test chamber
 408 on the sensor's response (S%) was evaluated at 60°C in the presence of 50 ppm H₂S gas, see Fig.
 409 8b. The results reveal that increasing the relative humidity inside the test chamber resulted in a
 410 decrease in the response of the sensors. An increase in the relative humidity up to 80% resulted in
 411 a 31.6% drop in the response of the sensors. This is expected because of the possible adsorption
 412 of water molecules onto the sensing membrane surface through the formation of H-bonding.
 413 Hence, the adsorption of H₂S molecules onto the surface of the sensors is limited by the H-bonds
 414 (Kruefu, Wisitsoraat, Tuantranont & Phanichphant, 2015).



422 **Fig. 8.** (a) Selectivity histogram for the PPy+5%IL+10 wt% WO₃-CA sensors for different gases
 423 and (b) dependence of the PPy-IL-10 wt% WO₃-CA sensors results on the humidity.

424 Table 1 contrasts the performance of the sensors developed in the current study is
 425 contrasted against those reported in the literature (Geng et al., 2006; Su & Peng, 2014; Geng,
 426 2010). The nanofiber and nanofilm-based sensors presented in this work exhibit a relatively
 427 excellent sensing performance compared with those studied previously. This is attributed to their
 428 unique composition and method of fabrication. The sensors presented in this work are able to
 429 operate at room temperature and yield a very low detection limit of 1 ppm and a fast response time
 430 of 22.8 s and 31.7 s for the nanofiber and nanofilm-based devices, respectively. This means that
 431 our sensors clearly outperform those requiring higher operating temperatures (90°C) and
 432 characterized by a longer response time (70-360 s).

434 **Table 1.** Performance comparison of the developed H₂S gas sensor with the literature for
 435 optimum response.

Composition/ material	Structure	Gas sensing Response (%)	Response Time	Detection limit [H ₂ S]	Operating temperature	Reference
CA-PPy-IL-10 wt% WO ₃	Nanofibers	31.2	22.8 (s)	1 ppm	20 (°C)	This work
CA-PPy-IL-10 wt% WO ₃	Nano film	25.5	31.7 (s)	1 ppm	20 (°C)	This work
PPy- WO ₃	Film	81	360 (s)	1 ppm	RT (°C)	[44]
PPy-3 wt% WO ₃	NCs	61	70 (s)	100 ppm	90 (°C)	[45]
PPy-1 wt% WO ₃	Film	49.55	NA	1000 ppm	90 (°C)	[60]

436

437 **3.5. Gas sensing mechanism**

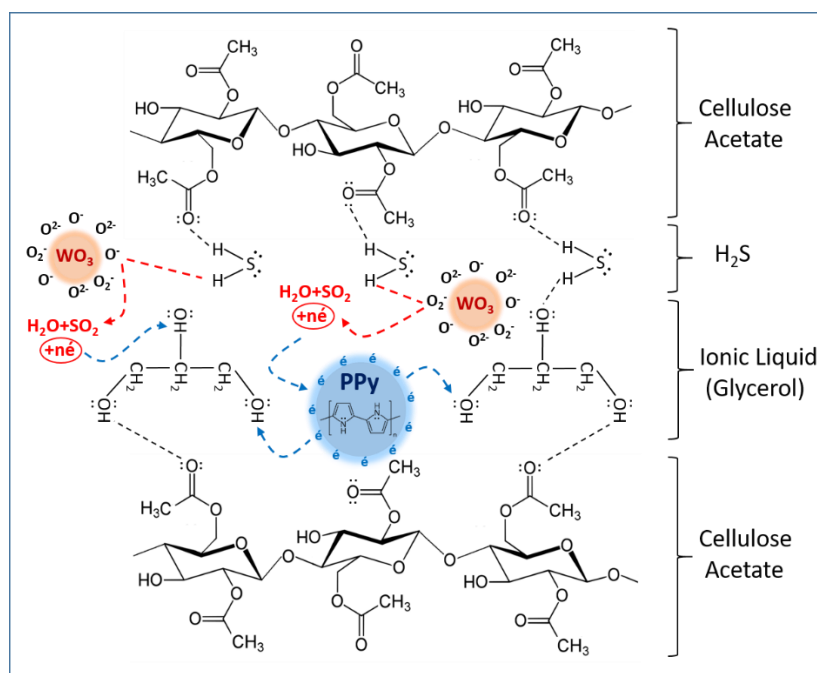
438 The sensing mechanism of semiconductor gas sensors is identified as a surface-controlled in which
 439 the particle size, surface states, and oxygen adsorption play an important role in the overall sensing
 440 mechanism (Rothschild & Komem, 2004; Rout, Hegde & Rao, 2008). The interaction between the
 441 target gas and the surface of the sensing material is the main reason behind the change of the sensor
 442 response (Hittini et al., 2020). Therefore, understanding the sensing mechanism for the proposed
 443 IL-PPy-WO₃ NPs-CA based sensor is necessary. Generally, when the sensor is exposed to H₂S, it
 444 interacts with the gas through the oxygen molecules adsorbed on the surface of the sensing
 445 material. As a result, the electrical conductivity (resistance) of the sensing material changes and
 446 the variation is detected as a readable current variation as a function of time (Ali, Awwad, Greish,
 447 Abu-Hani & Mahmoud, 2020). Initially, the oxygen molecules easily adsorb on the surface of the
 448 sensing material; because of their high electron affinity (0.43 eV) (Mane, Suryawanshi, Kim &
 449 Moholkar, 2016). The oxygen molecules adsorbed attract electrons from the IL-PPy-WO₃NPs-CA
 450 surface. Therefore, oxygen ions adsorbed (O_2^- , O^{2-} and O^-) appear on the sensor's surface. The
 451 following reactions occur on the sensing material surface (Rout, Hegde & Rao, 2008; Mane,
 452 Suryawanshi, Kim & Moholkar, 2016):



457 When the sensors (nanofibers and nanofilms) produced are exposed to H₂S, the oxygen molecules
 458 adsorbed interact with H₂S gas, which extract electrons from the conduction band of the WO₃ NPs
 459 and trap them at the surface in the form of ions as described in the following reaction (Su & Peng,
 460 2014; Hosseini, Iraji zad & Mortezaali, 2015):



462 The free electrons released are transferred within the matrix of the composite sensor via the H-
 463 bonding network between the remaining components of the sensor; namely the CA matrix (fiber
 464 or film), the PPy conducting particulates and the ionic liquid. This results in an overall increase in
 465 the conductivity of the sensor, as illustrated schematically in Fig. 9. A similar pattern was
 466 previously observed in a composite sensor that was composed of a chitosan matrix in addition to
 467 WO₃ NPs and IL (Ali, Awwad, Greish, Abu-Hani & Mahmoud, 2020).



468
 469 Fig.9. Illustration of the combined contribution of the sensor's components leading to the
 470 enhanced sensing of H₂S gas through H-bonding and e-transfer.

471 On the other hand, when the H₂S gas flow is turned off, the number of free electrons decreases and
472 leads to a reduction in the conductivity of the sensing element, causing a reversible sensing
473 behavior (Abu-Hani, Greish, Mahmoud, Awwad & Ayesh, 2017). The synergistic effect resulting
474 from the co-existence of PPy particulates, WO₃ nanoparticles and a well-established ionic liquid
475 in a matrix that compliments the integration of these components, is considered as the key reason
476 behind the exceptional properties of the proposed sensors (Su & Peng, 2014; Geng, 2010).

477 **4. Conclusion**

478 High-response and room-temperature sensors for H₂S gas detection were successfully fabricated
479 using electrospun nanofibers and solution-casting nanofilms. The proposed sensor assembly
480 consists of cellulose acetate blended with glycerol as an ionic liquid, mixed with a conducting
481 polymer and doped with tungsten oxide nanoparticles. The results of this study confirm that the
482 proposed sensors possess excellent sensing properties, a fast response time and a low detection
483 limit (1 ppm) even at room temperature. The results also demonstrate that the sensors exhibit high
484 selectivity for H₂S gas, long-term stability, and low power consumption. It was also shown that
485 nanofibers-based sensors are more sensitive and selective to detecting H₂S compared with the
486 nanofilm based sensor.

487 The lowest operating temperature for both nanofibers and nanofilm based sensors was 20°C, with
488 a minimum gas detection limit of 1 ppm. Moreover, both sensors exhibited a reasonably fast
489 response. For instance, for 2wt.% PPy+5%IL+10wt.% WO₃-CA, the average response time is 22.8
490 ± 1.05 s for nanofibers-based sensors and 31.7±1.3 s for the nanofilm-based sensors. A
491 comparative study with the literature shows that the sensors produced in this work outperform
492 other sensors, which often operate at a higher temperature (90°C) and require a longer response
493 time (70-360 s). The reliability of the sensors was also studied in terms of reproducibility and long-
494 term stability. For a given temperature (e.g. T= 40°C) and H₂S (1 ppm) gas, the repeated response
495 of each sensor was very close to the initial value recorded. This indicates the excellent
496 reproducibility and long-term stability of the proposed nanofibers and nanofilms-based sensors.
497 The dependence of the sensor's response S(%) on the relative humidity inside the test chamber at
498 60°C and 50 ppm was also evaluated. The results revealed a low humidity dependence of the
499 sensors since a reasonable drop in the response occurs only when the relative humidity increases
500 to 80%. Such distinctive properties of the sensors that are based environmentally friendly
501 materials can pave new paths for the development of reliable H₂S sensor to monitor indoor/outdoor
502 pollution.

503

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