

1 Nano-powder coating can make fault surfaces smooth and
2 shiny: implications for fault mechanics?

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6 Field and microstructural observations on exhumed, inactive, fault segments in
7 plate margin systems show that most of the upper crustal slip occurs in zones with a
8 thickness of less than a few tens of mm (Chester et al., 1993; Wibberley and Shimamoto,
9 2003). Slip zones in carbonate rocks show extreme slip localization within zones of less
10 than a few hundreds of microns, commonly bounded by sharp principal slip surfaces
11 which accommodate most seismic slip during earthquakes (De Paola et al., 2008;
12 Fondriest et al., 2012; Smith et al., 2011).

13 Siman-Tov et al. (2013, p. 703 in this issue of *Geology*) observed that carbonate
14 faults along the active Dead Sea Transform are characterized by naturally polished,
15 reflective and glossy surfaces, termed fault mirrors (FMs). At the microscale, the FM slip
16 zones consist of a <1 μm layer of tightly packed nanoscale grains, coating a thicker layer
17 made of twinned and elongated μm -size calcite crystals, produced by plastic deformation.
18 Siman-Tov et al. propose a ‘plastic-brittle’ mechanism to explain the formation of
19 nanoparticles, whose nanosize is controlled by the “long” and “thin” beams of calcite
20 crystals plastically deformed by twinning, and broken into nano-grains by brittle
21 deformation. The nanograin layer localizes slip and deforms by bulk ductility. Other
22 models proposed to produce nanograins rely on chemical-physical reactions triggered by

23 frictional heating (De Paola et al., 2011; Han et al., 2010; Han et al., 2007) or shock-
24 waves (Sammis and Ben-Zion, 2008), due to fast sliding during an earthquake. FMs have
25 extremely smooth surface topography, with mean roughness of <100 nm for lateral scales
26 below 550 nm (Siman-Tov et al., 2013). They are characterized by a Rayleigh roughness
27 and a different structure at scales <1 μ m (Siman-Tov et al., 2013), compared to the self-
28 affine roughness ranging from a few μ m to km, as seen in studies on polished principal
29 slip surfaces (Sagy et al., 2007). Siman-Tov et al. characterized the attributes and
30 roughness of FM surfaces at the sub- μ m scale, largely overlooked in previous studies, but
31 critical in controlling the frictional behavior of faults.

32 The friction between sliding fault surfaces controls the initiation, propagation and
33 termination of slip during earthquakes (Scholz, 1998). Leonardo Da Vinci first
34 recognized that friction on the contact surface between sliding bodies is related to the
35 ratio between the applied normal (F_n) and tangential shear (F_s) forces. Amontons (1699)
36 observed that the friction between two sliding bodies does not depend on the macroscopic
37 contact area, A , and that the shear force F_s is linearly proportional to the applied normal
38 force, F_n , with the constant of proportionality, the sliding friction coefficient $\mu = F_s/F_n$
39 (Amontons' Law). The applied F_n is supported by a real contact area, A_r , made by a
40 population of microcontacts (e.g., asperities), a small fraction of the macroscopic
41 contact area A (i.e., $A_r \ll A$) (Bowden and Tabor, 1950). According to this adhesion
42 theory, plastic yielding at asperities is expected as normal stresses approach the material
43 yield strength. The effective shear strength of welded asperities must be overcome to
44 slide. The main goal of adhesion theory is to develop a conceptual framework explaining

45 why macroscopic friction μ does not depend on the macroscopic contact area A , and why
46 the macroscopic F_s is linearly proportional to the applied F_n (Scholz, 2002).

47 The conceptual framework of adhesion theory applies to the rate and state theory
48 of friction, explaining the observed velocity and time dependence (Dieterich, 1979;
49 Ruina, 1983), controlling the initiation of unstable sliding and earthquake nucleation, and
50 mechanical healing of faults necessary to reset fault strength between failure events
51 (Marone, 1998; Scholz, 1998). Static friction increases with the logarithm of time,
52 interpreted as being due to the increase of contact area with contact age during
53 interpenetration and creep of asperities, while contact size distribution is insensitive to
54 time and normal stress (Dieterich and Kilgore, 1994). Sliding friction is velocity-
55 dependent, and with a change in velocity evolves to new steady-state values over a finite
56 critical slip distance, D_c (Dieterich, 1979; Ruina, 1983; Marone, 1998). D_c might be the
57 slip necessary to renew a surface contact and scales with the sliding surface roughness
58 (Marone, 1998). The conceptual framework of adhesion theory has been widely used to
59 explain macroscale frictional behavior, but deviations from single asperity theories have
60 sometimes been observed at the nanoscale, and attributed to the break-down of
61 continuum mechanics (Mo et al., 2009; Szlufarska et al., 2008) or to changes in chemical
62 bonding (Li et al., 2011). Whether asperity models can describe the behavior of contact
63 asperities at the nano-scale becomes relevant to the case of natural principal slip surfaces
64 with features similar to FMs (Siman-Tov et al., 2013).

65 Laboratory friction experiments under low slip rates (a few $\mu\text{m/s}$), displacements
66 (<1 cm) and temperatures ($T = 25$ °C) (Byerlee, 1978) and static borehole stress
67 measurements in the brittle crust (Townend and Zoback, 2000) show that faults are

68 usually strong ($\mu = 0.6\text{--}0.85$; Byerlee's law). However, recent theoretical (Rice, 2006)
69 and experimental studies (Di Toro et al., 2011) suggest that the coseismic frictional
70 strength of faults is much lower ($\mu = 0.1\text{--}0.3$) than predicted by Byerlee-type, low-
71 velocity experiments, when slip velocities and displacements are ~ 1 m/s and a few m,
72 respectively. Friction decreases with fault roughness for submicron size asperities, due to
73 abrasion by brittle fracture (Byerlee, 1967). Thus, the smoothness of the slip surfaces
74 could explain the weakening observed during friction experiments at seismic slip rates
75 (~ 1 m/s), where reflective, glossy FMs-like slip surfaces were produced (Han et al., 2010;
76 Han et al., 2007; Smith et al., 2013). Flash heating may be a viable mechanism for
77 dynamic weakening in seismic faults on theoretical (Beeler et al., 2008; Rice, 2006) and
78 experimental (Goldsby and Tullis, 2011) grounds. The operation of flash heating in
79 natural seismic faults with FMs-like ultra-smooth nature (Siman-Tov et al., 2013) could
80 be questioned, as unrealistically high slip rates would be required for surfaces with such
81 nanoscale asperities (Han et al., 2010,2011; De Paola et al., 2011; Tisato et al., 2012).

82 Asperity sliding may occur by shearing through the interlocked asperities and
83 large amount of wear are predicted and commonly observed along natural fault surfaces
84 (Scholz, 2002). During recent friction experiments performed in granite rocks at sub- and
85 seismic slip rates, fault lubrication has been observed when a critical gouge layer
86 thickness is reached, and able to act as a "third body" type lubricant which separates the
87 two sliding surfaces (Reches and Lockner, 2010). FM-like slip surfaces were also formed
88 during friction experiments performed at seismic slip rates in carbonate rocks, when
89 dramatic fault lubrication was also observed and interpreted as being due to the
90 development of nano-powders of lime coating the sliding surfaces (Han et al., 2010).

91 Further experimental work performed at fast slip rates on nano-powders has shown that
92 such materials can coat FM-like slip surfaces, making them very smooth; rounded
93 nanoparticles can start rolling along them rather than sliding, switching from high sliding
94 friction to low rolling friction (Han et al., 2011). However, nanopowder friction is
95 strongly rate-dependent, as at low slip rates these materials display a high friction (Han et
96 al., 2011); the role played by adhesion at low slip rates needs to be further investigated.
97 The nano-powders coating the natural FMs slip surfaces (Siman-Tov et al., 2013) could
98 act as a solid lubricant, in a similar fashion to what is observed in industry and inferred
99 from FMs produced during friction experiments at seismic slip rates. Granular lubricants
100 (particle size ~ 1 mm) consist of dry, cohesionless hard particles, and powder lubricants
101 (particle size ~ 1 μm) of dry, cohesive, soft particles (Worniyoh et al., 2007). During
102 sliding at low slip rates, granular particles undergo nearly elastic collisions and can slip,
103 roll and collide with the surface, whereas powders undergo completely inelastic collision
104 and can coalesce, producing a thin lubricating film protecting tribo-surfaces (Worniyoh et
105 al., 2007). The frictional behavior of nano-powders at low and high seismic slip rates,
106 however, is poorly understood and should be vigorously investigated, as they may hold
107 the key to what controls the structure and frictional behavior of seismic fault zones
108 (Siman-Tov et al., 2013).

109 Overall, Siman-Tov et al. will stimulate future studies of natural fault surfaces
110 trying to understand the interplay between plastic/ductile and brittle deformation and its
111 role in producing nanopowder coatings. It remains at present unclear whether FMs are
112 unambiguous indicators of seismic slip. Future experimental work should be aimed at
113 characterizing frictional properties and behaviors of nano-powders and smooth surfaces

114 for a range of pressures, temperatures, pore fluid pressures, and slip rates typical of brittle
115 crust faults. The challenge will be to bridge the gap between the mechanisms controlling
116 the frictional behavior of faults at the macro-, micro-, and nano-scale.

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