



Step-drawdown tests and the Forchheimer equation

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Is groundwater flow ever turbulent?



Figure 1: Results from a permeameter experiment on a quarry carbonate rock (after Moutsopoulos et al., 2009). Darcy's law (*q* linearly proportional to *J*) is known to work badly for high velocities.

Forchheimer equation

By consideration of data such as shown in Figure 1, Forchheimer (1901) suggested the quadratic alternative to Darcy's Law :

$$\frac{\mu q}{k} + \rho b q^2 + \frac{dP}{dx} = 0$$

where $k [L^2]$ is permeability $\mu [ML^{-1}T^{-1}]$ is dynamic viscosity $P [ML^{-1}T^{-2}]$ is fluid pressure x [L] is distance $\rho [ML^{-3}]$ is fluid density $b [L^{-1}]$ is the Forchheimer parameter

From a dimensional analysis Ward (1964) established that

 $b = f(k^{-1/2})$

From an empirical analysis Geertsma (1974) proposed that $b = 0.005\phi^{-5.5}k^{-0.5}$

where ϕ [-] is porosity.



Figure 4: Permeameter data that supports the Geertsma correlation. Note that Geertsma only used his own data and that of Cornell and Katz for the linear regression.



Figure 2: Friction factor against Reynolds number, Re, for a variety of porous media (after Chilton and Colburn, 1931). For pipe flow, turbulent flow occurs when Re > 2000. For porous media people say Re > 40.

Step drawdown tests

A common way to test a well is to pump at sequentially increasing rates; a step drawdown test. After a certain amount of time, drawdown in the well, s_w , reaches a quasi - steady value. These drawdowns are plotted against pumping rate, Q_w , and a quadratic is fitted (the Jacob Method): $s_w = AQ_w + BQ_w^2$

where *A* and *B* are known as the formation loss and well loss factors, respectively. Comparison with the large - time solution for Forchheimer flow to a well (Mathias et al., 2008)

$$_{w} \approx \frac{Q_{w}}{4\pi T} \left[\ln \left(\frac{4Tt}{Sr_{w}^{2}} \right) - 0.5772 \right] + \frac{bQ_{w}^{2}}{(2\pi H)^{2}r_{w}g}$$

where

S.

H [L] is formation thickness *t* [T] is time $T = Hk\rho g/\mu$ [L²T⁻¹] is transmissivity $S = H\phi(c_r + c_w)\rho g$ [-] is storativity

 r_w [L] is well radius

g [LT⁻²] is gravity

 c_r, c_w [M⁻¹LT²] are rock and fluid compressibility

suggests that $B = \frac{b}{(2\pi H)^2 r_w g}$ so field - scale estimates of *b* can be obtained from values of *B*.



Figure 5: Plot of quasi-steady drawdown, s_w , against corresponding pumping rate, Q_w , for the step drawdown test data shown in Figure 6.



Figure 3: A simple example showing that when one considers a scheme when water is produced from a single fracture, Re becomes independent of fracture aperture, *a*. The example illustrates one of many problems with applying Re to understanding groundwater flow.



Figure 6: Step drawdown test in a confined sandstone aquifer after Clark (1977).



Figure 7: Step drawdown test in a fractured sandstone aquifer (after van Tonder, 2001).

Further reading

Mathias, SA & Todman, LC 2010. Step-drawdown tests and the Forchheimer equation. Water Resources Research 46: W07514.

Mathias, SA, Butler, AP & Zhan, HB 2008. Approximate solutions for Forchheimer flow to a well. Journal of Hydraulic Engineering - ASCE 134(9): 1318-1325.